

Plane waves in a thermally conducting viscous liquid

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Abstract. The aim of this paper is to investigate plane waves in a thermally conducting viscous liquid half-space with thermal relaxation times. There exist three basic waves, namely; thermal wave, longitudinal wave and transverse wave in a thermally conducting viscous liquid half-space. Reflection of plane waves from the free surface of a thermally conducting viscous liquid half-space is studied. The results are obtained in terms of amplitude ratios and are compared with those without viscosity and thermal disturbances.

Keywords. Thermally conducting; viscous liquid; plane waves; reflection; amplitude ratios; thermal relaxation times.

1. Introduction

The study of stress waves is of central interest to the engineers, geophysicists and seismologists due to its varied applications. The extensive literature on the subject is reviewed in the books of Ewing *et al* (1957), Bullen (1963), Bath (1968), Miklowitz (1966), Achenbach (1973), Kalski (1963) and by many other authors. The problems of wave and vibration become more interesting in the field of seismology, when we study the problems with the additional parameters (e.g. viscosity, thermal disturbance, porosity, microrotation, anisotropy, etc.).

Chadwick & Sneddon (1958) and Lockett (1958) studied the propagation of thermoelastic plane waves. Knot (1899) derived the general equations for reflection and refraction at plane boundary. In classical dynamical-coupled theory of thermoelasticity, thermal and mechanical waves propagate with an infinite velocity, which is not physically admissible. To overcome this contradiction, the coupled theory of thermoelasticity has been extended by including the thermal relaxation time in constitutive relations by Lord & Shulman (1967) and Green & Lindsay (1972). Some problems on reflection in thermoelastic solid have been discussed by Deresiewicz (1960), Sinha & Sinha (1974) and Singh (2000).

The present paper deals with the plane wave propagation in a thermally conducting viscous liquid half-space with thermal relaxation times. The reflection of the plane waves from the free surface of a thermally conducting viscous liquid half-space is discussed.

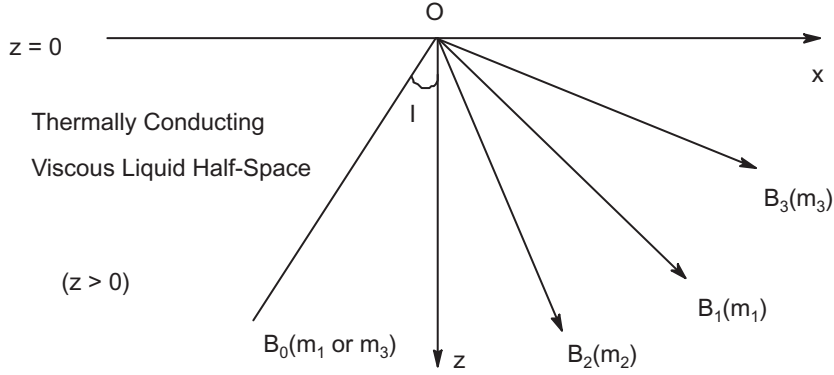


Figure 1. The geometry of the problem showing incident and reflected waves.

2. Formulation of the problem

We introduce rectangular Cartesian co-ordinates (x, y, z) and place the origin at the free surface of a thermally conducting viscous liquid half-space as shown in figure 1. The positive z -axis is taken into the half-space. Heat sources, external force loading and body forces are assumed to be absent. The constitutive equation and the equation of motion for a thermally conducting viscous liquid are (Lord & Shulman 1967; Green & Lindsay 1972)

$$t_{kl} = \left(K - \frac{2}{3}\eta\frac{\partial}{\partial t} \right) u_{i,i}\delta_{kl} + 2\eta\frac{\partial}{\partial t} e_{kl} - \beta(T + \tau_1\dot{T})\delta_{kl}, \quad (1)$$

$$\left(K + \frac{4}{3}\eta\frac{\partial}{\partial t} \right) \nabla(\nabla \cdot \mathbf{u}) - \eta\frac{\partial}{\partial t} \nabla \times (\nabla \times \mathbf{u}) - \beta\nabla(T + \tau_1\dot{T}) = \rho\ddot{\mathbf{u}}, \quad (2)$$

$$\rho C^*(\dot{T} + \tau_o\ddot{T}) + \beta T_o[\dot{u}_{i,i} + \Delta\tau_o\ddot{u}_{i,i}] = \kappa\nabla^2 T, \quad (3)$$

where K is bulk modulus, ρ is fluid density, η is fluid viscosity, T is temperature variable, T_o is absolute temperature, $\beta(= 3K\alpha_t)$ is thermal constant, α_t is coefficient of linear expansion, \mathbf{u} is displacement vector, t_{ij} and e_{ij} are stress and strain tensors, δ_{ij} is Kronecker delta, τ_o and τ_1 are relaxation times, κ is coefficient of thermal conductivity, C^* is specific heat at constant strain and the symbol Δ in (3) makes these fundamental equations possible for the two different theories of the generalized thermoelasticity.

For the LS (Lord–Shulman) theory $\tau_1 = 0$, $\Delta = 1$ and for GL (Green–Lindsay) theory $\tau_1 > 0$ and $\Delta = 0$. The thermal relaxation times τ_o and τ_1 satisfy the inequality $\tau_1 \geq \tau_o \geq 0$ for the GL theory only.

3. Solution of the problem

To solve the basic equations, we decompose the displacement vector as

$$\mathbf{u} = \nabla\phi + \nabla \times \psi, \quad \nabla \cdot \psi = 0, \quad (4)$$

Using (4), (2) reduces to

$$v_1^2 \nabla^2 \phi = \ddot{\phi} + \bar{\beta}(T + \tau_1\dot{T}), \quad (5)$$

$$v_2^2 \nabla^2 \psi = \ddot{\psi}, \quad (6)$$

where

$$v_1^2 = \left(K + \frac{4}{3} \eta \frac{\partial}{\partial t} \right) / \rho, \quad v_2^2 = \left(\eta \frac{\partial}{\partial t} \right) / \rho, \quad \bar{\beta} = \beta / \rho. \quad (7)$$

From (5), it is clear that the longitudinal wave is affected due to the thermal disturbances.

From equation (5), we have

$$T = (v_1^2 \nabla^2 \phi - \ddot{\phi}) / \bar{\gamma}, \quad (8)$$

where

$$\bar{\gamma} = \bar{\beta} [1 + \tau_1 (\partial / \partial t)], \quad (9)$$

Eliminating T from (3) and (8), we get

$$\begin{aligned} \nabla^4 \phi - \left[\frac{C^*}{\bar{\kappa}} \left\{ \left(1 + \tau_o \frac{\partial}{\partial t} \right) + \varepsilon \left(1 + \tau_1 \frac{\partial}{\partial t} \right) \left(1 + \Delta \tau_o \frac{\partial}{\partial t} \right) \right\} + \frac{1}{v_1} \frac{\partial}{\partial t} \right] \frac{\partial}{\partial t} \nabla^2 \phi \\ + \frac{C^*}{\bar{\kappa}} \frac{1}{v_1^2} \left(1 + \tau_o \frac{\partial}{\partial t} \right) \frac{\partial^3 \phi}{\partial t^3} = 0, \end{aligned} \quad (10)$$

where

$$\varepsilon = \bar{\beta}^2 T_o / v_1^2 C^*, \quad \bar{\kappa} = \kappa / \rho. \quad (11)$$

We assume the solution of (10) in the form

$$\phi = f(z) \exp [ik(ct - x)], \quad (c > v_1) \quad (12)$$

where k is the wave number.

With the help of (12), (10) reduces to

$$\frac{d^4 f(z)}{dz^4} + A \frac{d^2 f(z)}{dz^2} + B f(z) = 0, \quad (13)$$

where

$$A = k^2 \left(\frac{c^2}{v_1^2} - 2 \right) - kc(C^*/\bar{\kappa}) [(i - \tau_o kc) + \varepsilon_1 (i - \tau_1 kc)(1 + ikc\tau_o \Delta)], \quad (14)$$

$$\begin{aligned} B = k^4 \left(1 - \frac{c^2}{v_1^2} \right) + ck^3 (C^*/\bar{\kappa}) \left[(i - \tau_o kc) + \varepsilon (i - \tau_1 kc)(1 + ikc\tau_o \Delta) \right. \\ \left. - \frac{c^2}{v_1^2} (i - \tau_o kc) \right]. \end{aligned} \quad (15)$$

and phase velocity c is equal to $v / \sin I$, where v is the velocity of incident wave and I denotes the angle of incidence.

The solution of (13) is of the form

$$\begin{aligned} f(z) = A_1 \exp(ikm_1 z) + A_2 \exp(-ikm_1 z) + A_3 \exp(ikm_2 z) \\ + A_4 \exp(-ikm_2 z), \end{aligned} \quad (16)$$

where

$$m_1^2 = [(A^2 - 4B)^{1/2} + A]/2k^2, \quad (17)$$

$$m_2^2 = [-(A^2 - 4B)^{1/2} + A]/2k^2, \quad (18)$$

correspond to the longitudinal wave and thermal wave respectively and A_1, A_2, A_3, A_4 are arbitrary constants.

Equation (6) can be written as

$$v_2^2 \nabla^2 \psi = \ddot{\psi}, \quad (19)$$

where

$$\psi = (-\vec{\psi})_y.$$

We assume the solution of (19) in the form

$$\psi = g(z) \exp [ik(ct - x)], \quad (c > v_2). \quad (20)$$

From (19) and (20), the solution ψ can be written as

$$\psi = [A_5 \exp (ikm_3z) + A_6 \exp (-ikm_3z)] \exp [ik(ct - x)], \quad (21)$$

where

$$m_3^2 = (c^2/v_2^2 - 1), \quad (22)$$

corresponds to transverse wave and A_5, A_6 are arbitrary constants.

The displacement components of vector \mathbf{u} in x - z plane are

$$u_1 = \frac{\partial \phi}{\partial x} + \frac{\partial \psi}{\partial z}, \quad u_3 = \frac{\partial \phi}{\partial z} - \frac{\partial \psi}{\partial x}, \quad (23)$$

4. Reflection

We consider the propagation of plane waves in the x - z plane which makes an angle I with the normal to the boundary. For an incident longitudinal wave, $c = m_1 \operatorname{cosec} I$ and for an incident transverse wave, $c = m_3 \operatorname{cosec} I$. For incident longitudinal wave or transverse wave, we get three reflected waves in thermally conducting viscous liquid. The complete geometry showing these reflected has been given in figure 1.

The appropriate potentials are

$$\begin{aligned} \phi &= B_o \exp \{ik(ct - x + m_1z)\} + B_1 \exp \{ik(ct - x - m_1z)\} \\ &\quad + B_2 \exp \{ik(ct - x - m_2z)\}, \end{aligned} \quad (24)$$

$$\begin{aligned} T &= (1/\bar{\gamma}_o)[a_1 B_o \exp \{ik(ct - x + m_1z)\} + a_1 B_1 \exp \{ik(ct - x - m_1z)\} \\ &\quad + a_2 B_2 \exp \{ik(ct - x - m_2z)\}], \end{aligned} \quad (25)$$

$$\psi = B_o \exp \{ik(ct - x + m_3z)\} + B_3 \exp \{ik(ct - x - m_3z)\}, \quad (26)$$

where $B_i (i = 0, 1, 2, 3)$ are arbitrary constants, and

$$a_{1,2} = k^2 \{(c^2 - v_1^2) + m_{1,2}^2 v_1^2\}, \quad (27)$$

$$\bar{\gamma}_o = \bar{\beta}(1 + i\omega\tau_1), \quad (28)$$

Boundary conditions: For two-dimensional motion in x - z plane, the appropriate boundary conditions at free surface $z = 0$, are as

$$t_{zz} = 0, \quad t_{zx} = 0, \quad \partial T / \partial z = 0, \quad (29)$$

Making use of the potentials given by equations (24) to (26) in boundary conditions (29), after using the equations (1) and (23), we get a system of three non-homogeneous equations as

$$\sum_{j=1}^3 C_{ij} Z_j = d_j, \quad (i = 1, 2, 3) \quad (30)$$

where

$$\begin{aligned} C_{11} &= -(K + 4\eta i\omega/3)m_1^2 - (K - 2\eta i\omega/3) - \rho a_1/k^2, \\ C_{12} &= -(K + 4\eta i\omega/3)m_2^2 - (K - 2\eta i\omega/3) - \rho a_2/k^2, \quad C_{13} = 2\eta i\omega m_3, \\ C_{21} &= -2m_1, \quad C_{22} = -2m_2, \quad C_{23} = (1 - m_3^2) \\ C_{31} &= m_1 a_1, \quad C_{32} = m_2 a_2, \quad C_{33} = 0, \end{aligned}$$

and

For incident longitudinal wave

$$d_1 = -C_{11}, \quad d_2 = C_{21}, \quad d_3 = C_{31}, \quad (31)$$

For incident transverse wave

$$d_1 = C_{13}, \quad d_2 = -C_{23}, \quad d_3 = C_{33}, \quad (32)$$

and (Z_j) are the amplitude ratios for various reflected waves.

5. Numerical analysis

To explain the analytical procedure presented earlier, we now consider a numerical example. The results depict the variation of the angle of incidence with the modulus of the amplitude ratios.

The physical constants are (Fehler 1982)

$$\begin{aligned} \rho &= 1.01 \text{ gm/cm}^3, \quad K = 0.0119 \times 10^{11} \text{ dyne/cm}^2, \quad \eta = 0.0014 \text{ gm/cm s}, \\ K^* &= 0.48 \text{ cal/cm s}^\circ\text{C}, \quad C^* = 0.206 \text{ cal/gm}^\circ\text{C}, \quad T_o = 20^\circ\text{C}, \\ \omega &= 5s^{-1}, \quad \varepsilon = 0.053, \end{aligned}$$

Nayfeh & Nasser (1971) took $\tau_o = 3K^*/\rho C^* \alpha^2$. The relaxation time τ_1 is considered to be of same order as that of τ_o . The system of equations (30) is solved for amplitude ratios by using a computer program of the Gauss elimination method. The amplitude ratios for reflected longitudinal wave, reflected thermal wave and reflected transverse wave are computed for angle of incidence varying from 0° to 90° .

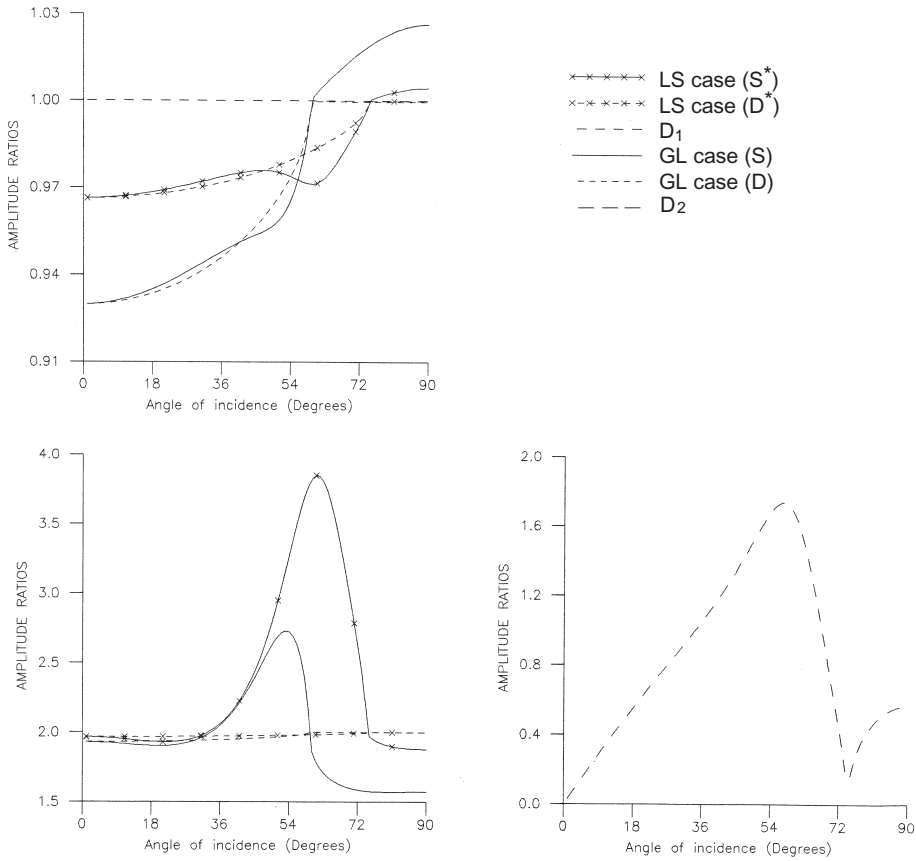


Figure 2. Variations of the amplitude ratios for incident longitudinal wave.

5.1 Incident longitudinal wave

The amplitude ratios for reflected longitudinal wave for Lord and Shulman (LS) case (Lord & Shulman 1967) and Green and Lindsay (GL) case (Green & Lindsay 1972) are shown by solid curves S^* and S in figure 2(a). These curves reduce to dashed curves D^* and D , if we put $\eta = 0$. If we neglect thermal effects, the curves D^* and D reduce to curve D_1 .

The amplitude ratios for reflected thermal wave first increase to their maximum values and then decrease sharply. The variations for LS and GL cases are shown by curves S^* and S in figure 2(b). These curves reduce to curves D^* and D , if we neglect viscous effect. This reflected wave would disappear, if we neglect thermal effect also.

The amplitude ratios for reflected transverse wave are shown by curve D_2 in figure 2(c). It increases to its maximum value and then oscillates. This reflected wave disappears, if we neglect viscous effect.

5.2 Incident transverse wave

The variations of the amplitude ratios for reflected longitudinal, thermal and transverse waves are shown in figure 3. The amplitude ratios for reflected transverse wave first decrease to its minimum value and then oscillate. The variations of amplitude ratios for reflected longitudinal

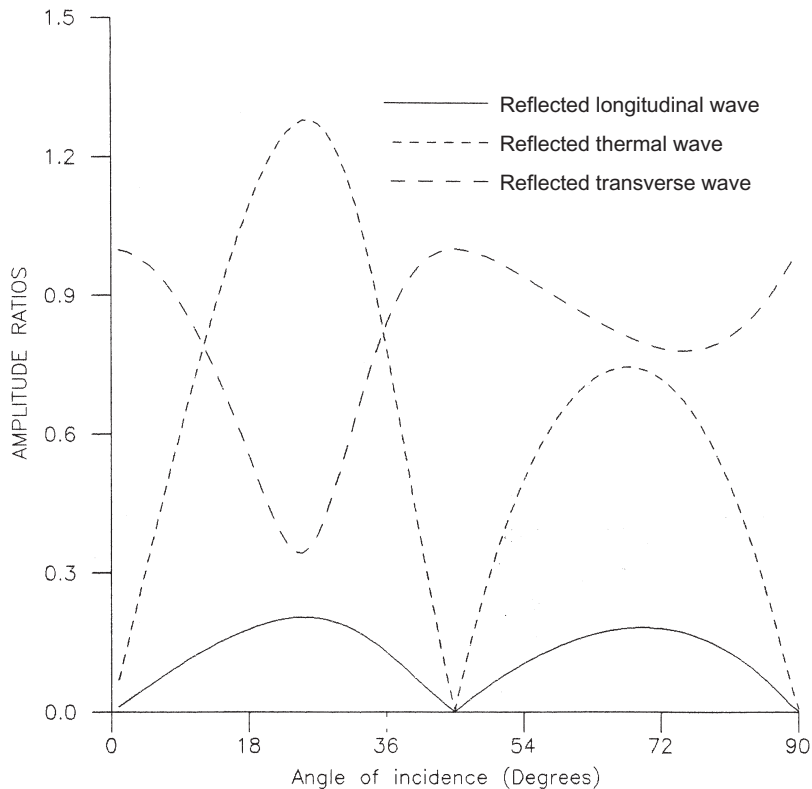


Figure 3. Variations of the amplitude ratios for incident transverse wave.

wave and reflected thermal wave are similar. They first increase to their respective maxima and then oscillate. The variation of the amplitude ratios for reflected longitudinal wave is shown after multiplying its original value by 10.

From § 5.1, we conclude that the reflected longitudinal and thermal waves are affected by second thermal relaxation in time and viscosity of the liquid. The reflected transverse wave will not exist if we put viscosity of liquid equal to zero. The analysis shown in this section is not possible in a non-viscous liquid.

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